Contactless river discharge from Unmanned Aerial Systems hydrometry: Performance evaluation using a large and diverse set of river cross sections **Xinqi Hu¹**, Zhen Zhou², Farhad Bahmanpouri³, Ye Tuo¹, Angelica Tarpanelli³, Silvia Barbetta³, David Gustafsson⁴, Daniel Wennerberg⁴, Karl Broich¹, Fabian Merk¹, Markus Disse¹, Peter Bauer-Gottwein⁵ 1 Chair of Hydrology and River Basin Management, Technical University of Munich, Germany, 2 DTU Space, Technical University of Munich, Germany, 2 DTU Space, Technical University of Denmark, 8 Research Council (CNR-IRPI), Via Madonna Alta 126, 06128 Perugia, Italy, 4 Swedish Meteorological and Hydrological Institute, 60176 Norrköping, Sweden, 5 Department of Geosciences and Natural Resource Management, University of Copenhagen, Øster Voldgade 10, 1350 Copenhagen Correspondence to: Xinqi Hu(xinqi.hu@tum.de) Study sites Background The river discharge measuremet is important, but it is... Torne Rive Hard to reach Even dangerous Time-consuming **Solution:** Unmanned Aerial Systems (UAS) hydrometry^[1] **Algorithm framework** Fig1 Overview of measured cross-sections **1** UAS hydrometry ^[2]: • WSE_IWR1443 ★ WSE_insitu 863.8 **6 Extreme Scenarios Analysis** Results Surface velocity: Doppler radar WSE accuracy Water penetrating radar River bathymetry: 1000 2000 River chainage (m) Algorithm performance in discharge calculation of discharg log law Water surface elevation (WSE): Radar altimetry power law 862.8 Conceptus entropy Accuracy of calculated discharge compared to gauge station records -40 -38 -36 -34 -30.0 -• DEM elevation: Lidar Percentage bias (%) 0.85 Entropy Log law **Power law** River average Water Surface(WPR) in-situ bathymet Water Surface(Altimetry) WPR bathymetey LiDAR elevation ntribution 47.84 All together 🛨 🛨 Doppler surface velo 46.95 72.88 7 -0.79 -0.78 50.09 48.03 -90.0 in-situ velocity uncertainty of **Doppler + WPR** discharge from ' -56.44 -54.28 -53.71 -61.50 -71.43 different input -13.50 -20.06 Percenta: 330.0 9 300.0 270.0 270.0 270.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 120.0 90.0 90.0 90.0 90.0 150.0 150.0 150.0 100.0 150.0 100.0 150.0 -3.94 8.40 Median -34.60 **2** Data processing: 25.06 24.45 Absolute Mea 22.83 34.13 26.68 49.59 47.84 50.09 Max 43.66 48.03 Torne -19.03 -40.03 -30.19 -61.61 -50.47 Min -0.81 -0.52 -0.55 -0.78 -0.58 -0.82 0 Surface velocity to bulk velocity Uncertainty -18.13 -12.82 -3.94 -0.42 -34.60 10.81 Median of input data - 0.85 model^[3] - Power law model^{[2} 19.63 22.78 Absolute Mear 15.94 16.15 31.71 Area Depth Width Froude WDratio Netted P WSS Area Depth Width Froude WDratio Wetted P WSS -60.0 Ma 72.88 40.14 - Log law model^[5] - Entropy model^[6] 46.95 40.01 41.81 Rönne å Max Fig5 Percentage change in calculated discharge under -42.07 -28.05 -21.84 11.88 -39.29 Mir Fig3 Pearson (left) and Spearman (right) correlation coefficients between cross-section Water surface slope from WSE extreme scenarios with ±30% biases applied to different 39.10 18.99 Median 28.31 -14.92 14.56 properties and (i) algorithm accuracy, (ii) discharge uncertainty, (iii) contributions of input 22.71 42.18 Absolute Mea 29.00 26.79 23.41 input combinations. V, H, and WSS represent surface uncertainties to discharge uncertainty, and (iv) input uncertainties. WPR represents river -33.67 -31.93 -35.21 -34.82 -32.72 Max velocity, water depth, and water surface slope, respectively. bathymetry measurements; Doppler refers to water surface velocity; altimetry indicates -61.50 -56.44 -53.71 -71.43 -54.28 Points are color-coded by river width. water surface elevation; WSS denotes water surface slope.On the x-axis, Hydraulic_R is the -44.23 -49.92 -39.09 -47.43 Median -50.41 The 0.85 method does not amplify or attenuate input data errors hydraulic radius, WDratio is the river width-to-depth ratio, Wetted P is the wetted 47.76 40.15 45.58 42.80 51.61 - water depth of i_{th} segment Absolute Mean during discharge calculation. The entropy method exhibits the perimeter, and WSS is the water surface slope. b_i - column width of i_{th} segment 1.975 1.950 1.950 925 • WR1443 • X5 location Fitted line uncertainty band • Fitted line • WSS line: -2.9234 ± 0.5261 cm/km • WSS ± 1 std omparison of calculated roughness values highest variability in error propagation. Extreme error cases for all - 1:1 Line Uncertainty of the discharge calculation Overall, the average discharge accuracy (MAPE) • Averaged result, MAPE:17.28% methods predominantly occur at cross sections with smaller widths. *WSS*- Water surface slope from water surface elevation: 0.85 method, MAPE:14.75% 68600 68800 Log law method, MAPE:25.52% across four methods is 24.45%. The average equals to friction slope under diffusive wave approximation Power law Method, MAPE:19.01% Entropy Method, MAPE:20.89% accuracy (MAPE) of roughness is 17.28%. The overall discharge uncertainty due to input _____ uncertainties ranges from 0% to 4%, expressed as the **3** Discharge calculation: At the river scale, the Torne River (large, flat) shows $Q = K_{\rm s} A R^{2/3} S_{\rm f}^{1/2}$ **Reference** standard deviation normalized by the ensemble mean the best performance with the 0.85 method; the [1] Bandini, F., Lüthi, B., Peña-Haro, S., Borst, C., Liu, J., Karagkiolidou, S., Hu, X., from Monte Carlo simulations (Fig. 4). Lemaire, G. G., Bjerg, P. L., & Bauer-Gottwein, P. (2021). A Drone-Borne Method to Bulk velocity(0.85, log Isar River (small, braided) performs the worst. For Geometry profile law, power law, entropy) Jointly Estimate Discharge and Manning's Roughness of Natural Streams. Water $U_{m,i}b_ih_i$ Smaller cross sections tend to exhibit highe $Q = \sum_{i=1}^{n}$ the Rönne å River (small, flat), the power law Resources Research, 57(2). Uncertainty Uncertainty Uncertainty uncertainties (Fig. 3). [2] Zhou, Z., Riis-Klinkvort, L., Ahrnkiel Jørgensen, E. et al. UAS hydrometry: contactless from WPR from Doppler from Altimeter method is best, with power law and log law river water level, bathymetry, and flow velocity - the Rönne river dataset. Sci Data 12. The contribution of surface velocity measurements to Discharge and outperforming 0.85 and entropy methods. K_s - Gauckler-Manning-Strickler coefficien - discharge discharge uncertainty increases with river depth, while [3] Hauet, A., Kruger, A., Krajewski, W. F., Bradley, A., Muste, M., Creutin, J.-D., & ghness estin At the cross-section scale (Fig. 3), the accuracy of Wilson, M. (2008). Experimental System for Real-Time Discharge Estimation Using an the contribution from water surface elevation **R** - hydraulic radius: R = S_f - friction slope: equals to WSS under Image-Based Method. Journal of Hydrologic Engineering, 13(2), 105-110 40 the 0.85 and entropy methods improves with larger decreases (Fig. 3). [4] Cheng, N.-S. (2007). Power-law index for velocity profiles in open channel flows. diffusive wave approximation 0.85 Method: Log law Method: Entropy Method Power law Method: ADCP estimated Manning – Strickler K_s Q, Q_std; Ks, Ks_std Q, Q_std; Ks, Ks_std Q, Q_std; Ks, Ks_std Q, Q_std; Ks, Ks_std Advances in Water Resources, 30(8), 1775-1784. cross sections, while the accuracy of the log law Cross sections with greater water depth or lower Fig2 Comparison of UAS-based and ADCP $U_{m,i}$ - vertical mean velocity of i_{th} water 5] Keulegan, G. H. (1938). Laws of turbulent flow in open channels. National Bureau of **4** - cross-sectional area and power law methods increases with higher column based roughness values, evaluated using Q, Q_std, Ks, Ks_std Fig4 Boxplot of uncertainty of calculated dischare 6] Chiu, C. L. (1988). Entropy and 2-D Velocity Distribution in Open Channels. Journal of Incertainties in surface velocity measurements (Fig. 3) Hydraulic Engineering, 114(7), 738-756. mean absolute percentage error (MAPE)

















River		Area(m²)	Depth (m)	Hydraulic radius(m)	Width (m)	Froude	Width/Depth ratio	Wetted perimeter (m)	Water surface slope(cm/km)		Torne Rive
Torne	Min	24.404	0.421	0.420	56.562	0.066	64.507	34.471	3.960		
	Max	1121.810	3.001	2.990	675.678	0.295	592.445	342.634	166.440		
	Median	464.893	1.369	1.367	286.995	0.129	189.386	141.468	10.930		
	Mean	505.764	1.517	1.515	335.186	0.142	248.541	181.046	35.623	the second second	
Rönne å	Min	9.032	0.531	0.525	16.135	0.068	13.566	11.664	2.923	and the second	Ronne Rive
	Max	48.710	1.771	1.700	37.275	0.359	31.804	17.188	193.804		
	Median	30.259	1.189	1.135	25.707	0.104	22.089	14.168	20.898		
	Mean	31.171	1.188	1.140	24.621	0.143	22.347	14.202	86.465		
lsar	Min	1.170	0.143	0.143	5.893	0.263	16.941	4.159	110.742	Care M	Isar River
	Max	5.172	0.348	0.338	31.498	0.883	219.802	13.375	534.695		
	Median	2.834	0.197	0.196	14.891	0.450	55.086	8.105	257.474		
	Mean	3.096	0.231	0.228	14.837	0.502	80.347	8.600	291.125		and the second se
Orco	Min	21.074	0.470	0.469	25.737	0.134	12.839	15.800	222.454		Orco Pivor
	Max	51.716	2.005	1.831	63.321	0.570	134.652	46.280	409.053	and the set	UICO MIVEI
	Median	32.572	0.777	0.766	34.262	0.323	45.940	23.796	337.969		
	Mean	35.720	0.981	0.942	41.246	0.344	58.258	25.928	326.307		
Ро	Min	101.004	1.047	1.040	78.866	0.096	61.685	44.740	10.706	TEN SULLA	
	Max	360.522	1.661	1.651	216.693	0.434	130.429	157.775	129.370	Share S	Po River
	Median	116.839	1.157	1.147	107.910	0.324	103.095	71.774	90.115		
	Mean	164.649	1.245	1.236	125.286	0.283	99.076	84.454	76.795	ANS A	











